

REPORT DOCUMENTATION PAGE				Form Approved OMB No. 0704-0188	
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing this collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number. PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.					
1. REPORT DATE (DD-MM-YYYY) 03-05-2006		2. REPORT TYPE Technical Paper		3. DATES COVERED (From - To)	
4. TITLE AND SUBTITLE  Investigation of Particle-in-Cell Acceleration Techniques for Plasma Simulations (PREPRINT)				5a. CONTRACT NUMBER	
				5b. GRANT NUMBER	
				5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S) David D. Marshall (California Polytechnic Univ.); Douglas B. VanGilder (AFRL/PRSS)				5d. PROJECT NUMBER 48470052	
				5e. TASK NUMBER	
				5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)  Air Force Research Laboratory (AFMC) AFRL/PRSS 1 Ara Drive Edwards AFB CA 93524-7013				8. PERFORMING ORGANIZATION REPORT NUMBER  AFRL-PR-ED-TP-2006-126	
9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES)  Air Force Research Laboratory (AFMC) AFRL/PRS 5 Pollux Drive Edwards AFB CA 93524-70448				10. SPONSOR/MONITOR'S ACRONYM(S)	
				11. SPONSOR/MONITOR'S NUMBER(S) AFRL-PR-ED-TP-2006-126	
12. DISTRIBUTION / AVAILABILITY STATEMENT  Approved for public release; distribution unlimited (AFRL-ERS-PAS-2006-090)					
13. SUPPLEMENTARY NOTES Presented at the 37 <sup>th</sup> AIAA Plasmadynamics & Lasers Conference, San Francisco, CA, 5-8 June 2006.					
14. ABSTRACT COLISEUM is an application framework that integrates plasma propagation schemes and arbitrary 3D surface geometries. Using Particle-in-Cell (PIC) schemes to model the plasma propagation high fidelity modeling of the plasma and its interaction with the surfaces is possible. In order to improve the computational performance of the Particle-in-Cell (PIC) scheme within COLISEUM (AQUILA), accelerate techniques have been developed that significantly decrease the amount of CPU time needed to obtain a steady-state solution. These schemes have been demonstrated to decrease the CPU time from 3 to 24 times with little appreciable differences in the global particle properties and number densities. This work investigates the differences in the local plasma properties that result from the application of the different acceleration techniques. In particular, the number densities and velocity distributions of the ions and neutrals demonstrate that the solution acceleration schemes produce very similar solutions outside the main path of the plasma source. Within the main path of the plasma source the local plasma properties show marked differences that might be associated with the time steps associated with these schemes and/or the collision modeling scheme within AQUILA.					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT  A	18. NUMBER OF PAGES  23	19a. NAME OF RESPONSIBLE PERSON Daron Bromaghim
a. REPORT Unclassified	b. ABSTRACT Unclassified	c. THIS PAGE Unclassified			19b. TELEPHONE NUMBER (include area code) N/A

# Investigation of Particle-in-Cell Acceleration Techniques for Plasma Simulations —PREPRINT—

David D. Marshall\*

*California Polytechnic State University, San Luis Obispo, CA 93407-0352, USA*

Douglas B. VanGilder<sup>†</sup>

*U.S. Air Force Research Laboratory, Edwards AFB, CA 93524-7680, USA*

COLISEUM is a application framework that integrates plasma propagation schemes and arbitrary 3D surface geometries. Using Particle-in-Cell (PIC) schemes to model the plasma propagation high fidelity modeling of the plasma and its interaction with the surfaces is possible. In order to improve the computational performance of the Particle-in-Cell (PIC) scheme within COLISEUM (AQUILA), accelerate techniques have been developed that significantly decrease the amount of CPU time needed to obtain a steady-state solution. These schemes have been demonstrated to decrease the CPU time from 3 to 24 times with little appreciable differences in the global particle properties and number densities. This works investigates the differences in the local plasma properties that result from the application of the different acceleration techniques. In particular, the number densities and velocity distributions of the ions and neutrals demonstrate that the solution acceleration schemes produce very similar solutions outside of the main path of the plasma source. Within the main path of the plasma source the local plasma properties show marked differences that might be associated with the time steps associated with these schemes and/or the collision modeling scheme within AQUILA.

## Nomenclature

$c$	Velocity, [m/s]
$c_i$	Three-dimensional velocity space, [m/s $\times$ m/s $\times$ m/s]
$c_r$	Relative velocity between two particles [m/s]
$f$	Velocity distribution function, [-]
$\dot{m}$	Mass flow rate, [kg/s]
$N$	Number of computational particles
$n$	Particle number density [m <sup>-3</sup> ]
$P$	Probability of collision
$S$	Surface of integration
$t$	Time, [s]
$T_e$	Electron Temperature [eV]
$\mathcal{V}$	Volume of computational cell [m <sup>3</sup> ]
$W_p$	Ratio of physical particles to computational particles
$x$	Position, [m]

## Subscripts

---

\*Assistant Professor, Aerospace Engineering Department, California Polytechnic State University, San Luis Obispo, CA 93407-0352, Member AIAA.

<sup>†</sup>Research Scientist, U.S. Air Force Research Laboratory, AFRL/PRSS, 1 Ara Road, Edwards AFB, CA 93524-7680, Member AIAA.

Copyright © 2006 by the American Institute of Aeronautics and Astronautics, Inc. All rights reserved.

max	Maximum value
$s$	Surface property

#### *Conventions*

NTC	No-Time-Counter Collision Model
SCN	COLISEUM cases run without subcycling
SCY	COLISEUM cases run with subcycling
VDF	Velocity Distribution Function

#### *Symbols*

$\phi$	Electrostatic potential [V]
$\sigma_T$	Total collision cross-section [m <sup>2</sup> ]
$\tau$	Characteristic time [s]

## I. Introduction

THE Air Force Research Laboratory has developed an application framework that integrates plasma propagation schemes with arbitrary 3D surface geometries<sup>1</sup> in order to investigate the interactions between the plasma plume from electric propulsion thrusters and the spacecraft. A hybrid Particle-in-Cell plasma model within COLISEUM, called AQUILA,<sup>2</sup> is the basis of this work. The COLISEUM framework is used to model the thrusters in space environment for prediction of the interactions and also to model the thrusters in vacuum chambers in order to validate the models used in COLISEUM against experimental data. In order to improve the computational performance of the AQUILA model, acceleration techniques have been developed that significantly decrease the amount of CPU time needed to get the simulation to a steady-state. These schemes have been demonstrated to decrease the CPU time by up to 24 times with little appreciable differences in the global particle properties.

Two previous studies have been performed on the acceleration schemes within COLISEUM. Gibbons et al.<sup>3</sup> also demonstrated the subcycling technique in which the slower moving neutrals are propagated at a larger time step than the faster moving ions. Gibbons et al.<sup>4</sup> demonstrated the use of the subcycling scheme with a scheme that decoupled the modeling of surface interactions from the plume propagation. It utilizes particle sources from the surfaces in place of the self-consistent surface interaction modeling. Both of these schemes are intended to provide increased convergence rates to a steady-state solution. The desire is to end up with the same final plasma distribution with or without the acceleration techniques. The present study intends to provide a detailed analysis of the resulting plasma properties and any differences in the local plasma properties that result from the application of the different acceleration techniques.

## II. Computational Techniques

This section provides a brief overview of the major computational techniques within COLISEUM. Consult the User's Manual for more details.<sup>5,6</sup>

### A. COLISEUM Framework

COLISEUM is a computational framework that provides a tool that can be used to model the interaction of plasmas with arbitrary surfaces in three-dimensional space.<sup>3</sup> These simulations can be of a plasma in a contained domain or in an open domain. This allows the simulation of experiments in vacuum chambers as well as plasmas in the low density space environment. The primary focus of COLISEUM is to investigate the erosion associated with the plasma particles impacting surfaces, known as sputtering. This sputtered material may be re-deposited on other surfaces. COLISEUM provides the integration of the CAD surface modeling, the plasma propagation, and the sputtering of material within one consistent framework.

#### 1. Surface Modeling

The surface model can be input in a variety of standard formats including ANSYS and ABAQUS formats. In addition, surface properties are also specified in order to differentiate the various materials that may compose each surface. In order to accurately model the sputtering, additional material information must be

specified that describes the interaction between particles that may be impacting surfaces and the material that the surfaces are composed of. This is known as the material interaction parameters in COLISEUM.

## 2. Plasma Modeling

The plasma modeling within COLISEUM has two major components to it. The first is the modeling of the source. Sources are surfaces within the geometry that particles will be emitted. To model sources, a velocity distribution function, VDF, must be specified throughout the surface of the source. In general, the VDF is a function of space, time, and obviously velocity,  $f(\vec{x}, \vec{c}, t)$ . This is used to determine the mass flow rate,  $\dot{m}$ , as

$$\dot{m}_s = \int_{\mathcal{S}} \int_{c_i} f_s(\vec{x}, \vec{c}, t) dc_i d\mathcal{S} \quad (1)$$

where  $c_i$  is the three-dimensional velocity space, and  $\mathcal{S}$  is the surface of the source. The VDF does not need to be specified in direction, as COLISEUM provides surface modules that model common sources: (1) user specified flux information typically from experimental data, (2) user specified flux and velocity information typically from experimental data, and (3) a shifted Maxwellian distribution with the velocity shift normal to the surface.

The second major component of the plasma modeling within COLISEUM is the plasma simulation itself. COLISEUM was developed with the idea of supporting any number of plasma modeling schemes. One of the original models is the prescribed plume model which simply imports the previously obtained plasma properties of the flow field. The particle fluxes on the surfaces are then directly obtained from this data. The other original model is the ray tracing model which traces the particle trajectory from the sources without accounting for the electrostatic potential field forces. The particle fluxes on the surfaces are then able to be determined.

As COLISEUM has matured, more sophisticated plasma modeling modules have been developed. DRACO from Virginia Tech<sup>7</sup> is a Cartesian cell based, finite-element PIC-DSMC simulation. AQUILA from MIT<sup>8</sup> is an unstructured tetrahedral cell based, finite-element PIC-DSMC simulation. It is AQUILA that is being used as the basis of this investigation.

## 3. Sputtering Modeling

The sputtering models in COLISEUM are based on standard models from Roussel et al.<sup>9</sup> and Gardner et al.,<sup>10</sup> Kannenberg et al.,<sup>11</sup> and Yamamura et al.<sup>12</sup> Coupling the sputtering models with the re-deposition process has been included in order to account for how the re-deposited material may itself induce sputtering. This allows a more accurate model of the final surface deposition characteristics.

## B. Particle Propagation Scheme

The time integration scheme used within AQUILA to propagate the plasma particles is the standard leap frog scheme<sup>13</sup> which is second order accurate in time. The electrostatic forces are modeled using the electrostatic potential equation with the inclusion of space-charge effects.<sup>8</sup> A finite element formulation is used to solve the potential equation with a Newton-method type scheme to handle the nonlinear nature of the resulting equations.

## C. Collision Modeling

The collision modeling within AQUILA<sup>14</sup> is based on the No-Time-Counter, NTC, method of Bird.<sup>15</sup> The probability of a collision between two particles is given as

$$P = \frac{W_p (\sigma_T c_r) \Delta t}{\mathcal{V}} \quad (2)$$

where  $W_p$  is the ratio of physical particles to computational particles,  $\sigma_T$  is the total collision cross-section,  $c_r$  is the relative speed between the two particles, and  $\mathcal{V}$  is the volume of the computational cell containing particles. Similarly, the maximum probability of a collision is

$$P_{\max} = \frac{W_p (\sigma_T c_r)_{\max} \Delta t}{\mathcal{V}} \quad (3)$$



The NTC scheme samples only a fraction of the total number of particle pairs in the computational cell, and similarly increases the probability of collision of each sampled particle pairs. Within COLISEUM, only  $P_{\max}N_pN_q$  particle pairs are chosen from species  $p$  and  $q$ . Thus, the lower the maximum probability of collision, the fewer collision samples are taken. The resulting collision probability for a sampled collision pair is then

$$P = \frac{\sigma_t c_r}{(\sigma_T c_r)_{\max}} \quad (4)$$

A simple accept/reject scheme can be used on this probability. Notice that this scheme will sample the appropriate number of collision pairs only when an accurate maximum probability has been determined. Therefore, this scheme will produce accurate collision rates only after a large number of collisions have occurred so that the maximum probability term has been reasonably determined.

#### D. Subcycling Scheme

The subcycling scheme within COLISEUM utilizes the fact that there is a significant difference between the collision times scales and the ion characteristic times. The ion characteristic time is based on the spatial resolution of the computational grid which is being used to model the electrostatic potential field. In order to keep the electrostatic forces on the particles varying smoothly as they travel through the domain, the ions should not travel more than a third of a cell within one time step. For the simulation to be modeled in this paper, the ion velocity is 20 km/s and the neutral velocity is 200 m/s. For characteristic length of the smallest volume as 0.01 m this results in the ion characteristic time of  $5 \times 10^{-7}$  s and the neutral characteristic time of  $5 \times 10^{-5}$  s. This is a factor of 100 difference between the two.

Using the following relations for the elastic collisions between neutrals and neutral ions<sup>16</sup> to characterize the collision cross-sections

$$\sigma_{Xe-Xe}^{\text{el}} = \frac{2.117 \times 10^{-18}}{c_r^{0.24}} \quad (5)$$

$$\sigma_{Xe-Xe^+}^{\text{el}} = \frac{8.2807 \times 10^{-16}}{c_r} \quad (6)$$

and for the charge-exchange collisions between neutrals and ions<sup>17</sup>

$$\sigma_{Xe-Xe^+}^{\text{cex}} = 1.1872 \times 10^{-20} [-23.3 \log(c_r) + 188.81] \quad (7)$$

a mean time to collision can be determined as

$$\tau = \frac{1}{n\sigma c_r} \quad (8)$$

Table 1 shows the characteristic times for the simulation to be modeled in this paper and a maximum particle number density of  $10^{18} \text{ m}^{-3}$ . Included in these calculations is the high speed neutrals that will result from previous charge exchange collisions. Thus, the neutrals in the collision calculations could have the low speed 200 m/s value or the high speed 20000 m/s value. Clearly a simulation time step less than  $4.7 \times 10^{-5}$  s is needed to resolve the collision time scales.

**Table 1. Collision Characteristic Times**

Collision Type	$c_r$ [m/s]	$\sigma$ [m <sup>2</sup> ]	$\tau$ [s]
Xe-Xe Elastic	200	$5.94 \times 10^{-19}$	$8.42 \times 10^{-3}$
Xe-Xe Elastic	10000	$2.32 \times 10^{-19}$	$4.28 \times 10^{-4}$
Xe-Xe Elastic	20000	$1.97 \times 10^{-19}$	$2.54 \times 10^{-4}$
Xe-Xe <sup>+</sup> Elastic	10000	$8.20 \times 10^{-20}$	$1.21 \times 10^{-3}$
Xe-Xe <sup>+</sup> Elastic	20000	$4.14 \times 10^{-20}$	$1.21 \times 10^{-3}$
Xe-Xe <sup>+</sup> Charge Exchange	10000	$1.13 \times 10^{-18}$	$8.73 \times 10^{-5}$
Xe-Xe <sup>+</sup> Charge Exchange	20000	$1.05 \times 10^{-18}$	$4.75 \times 10^{-5}$

Therefore, there is only one physical phenomena that requires a time step in the order of  $10^{-7}$  s, and that is capturing the electrostatic forces applied to the ions.

Computing one complete computational cycle encompasses the following steps

1. Subcycle Fast Particles
  - (a) Move Fast Particles
  - (b) Inject Fast Particles
  - (c) Update Electrostatic Fields
2. Move Slow Particles
3. Inject Slow Particles
4. Perform Collisions

By only moving the slow particles a fraction of the number times that the fast particles must be moved as well as performing the collisions on the coarse time step a significant amount of computational effort is saved.

### E. Velocity Distribution Function Probe

In order to determine the local plasma properties, a new probe was introduced into the COLISEUM probe architecture. This probe samples a region in space (currently a computational cell) and stores the velocity of every particle of a specified type that resides within the cell. The frequency of sampling can be adjusted as well as the start and end times of the sampling. Once the sampling is completed, the probe sorts the particles into bins of user specified sizes. The results can be written out as a table of the non-empty bins, or as a Tecplot formatted structured grid data file. Further processing is possible with this data if only binning on particle speed is desired.

## III. Results

The following results are all for the same test problem. First, solution convergence is demonstrated by using a fine time step, that is on the order of the characteristic time step of the electrostatic forces, and demonstrating that further refinement of the time step does not result in any appreciable change in the solution. Second, a solution is presented with a coarse time step, that is on the order of the collision time scale, and is compared to the fine time step solution. Next, a solution is presented using the subcycling scheme discussed above, with the ions moving at the fine time step and the neutrals moving at the coarse time step.

### A. Test Problem Description

The test problem is a highly simplified geometry based on a plasma source within a vacuum chamber. Figure 1 shows the surface meshes associated with the test problem. The plasma source is a small cylinder with the cylinder axis aligned with the z-axis. The plasma is emitted in the positive z-direction from that particular face of the cylinder. The vacuum chamber is simplified to a cylinder with the cylinder axis again aligned with the z-axis. The plasma source is firing at one end of the cylinder and the other end of the cylinder is a particle sink such that any particle that hits that surface leaves the computational domain.

The chamber has a diameter of 1.5 m and a length of 2 m. The plasma source has a diameter of 0.1 m and a length of 0.1 m. The distance between the plasma source face and the chamber face is 1.3 m.

The plasma source is composed of two particle types, a low speed neutral and a high speed ion. Both are modeled using the drifting Maxwellian source model within COLISEUM.<sup>5</sup> The neutral drift velocity is 200 m/s and temperature is 700 K. The ion drift velocity is 20 km/s and temperature is 10 eV.

The electrostatic potential is modeled using the quasi-neutral model within AQUILA.<sup>14</sup> This applies the quasi-neutrality assumption and inverting Boltzmann's equation to obtain an expression for the electrostatic potential

$$\phi = \phi_0 + \frac{kT_e}{e} \ln \left( \frac{n_e}{n_{e0}} \right) \quad (9)$$

where the electron temperature,  $T_e$ , is set to 2 eV and the reference electron number density and potential is specified to be at a potential of 0 V just in front of the thruster face.

In order to examine the similarities of the local properties of the plasma between the three cases, the velocity distribution for the neutrals and ions were obtained 0.1 m in front of the plasma source as well as 0.28 m above the thruster face. The first sampling will examine the plume modeling capabilities, while the second sampling will examine the capabilities to model the plasma outside of the plume.

The computer that these simulations were performed for the timing results is a dual processor AMD Opteron 242 system with 2 GB of RAM with an additional 2 GB of swap space. Use of the machine was minimized while the cases were running, and all cases resided in physical memory, so the swap space was not utilized except to move other non-essential applications out of RAM at the start of the simulation.

In order to quickly distinguish between the various cases to be run, the acronym SCN will designate cases without the use of subcycling and SCY will designate the cases with subcycling.

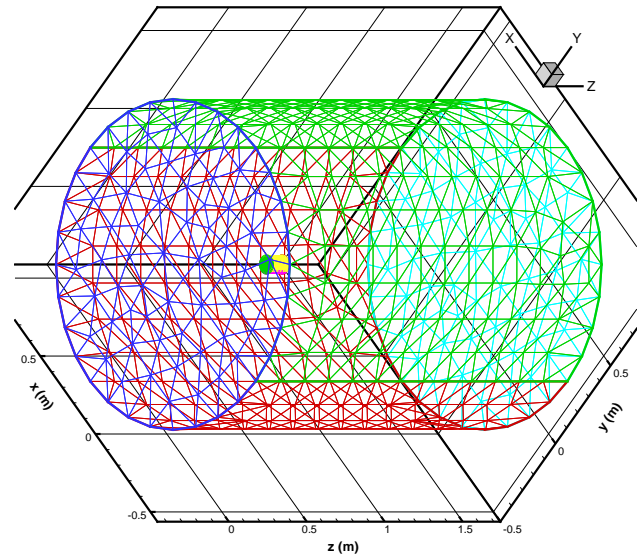


Figure 1. Simple Chamber Geometry

## B. Solution Convergence Demonstration

With the baseline fine time step for this simulation established as  $2.5 \times 10^{-7}$  s, three cases were run to demonstrate the convergence of the solution at this time step. One case was at twice the baseline time step,  $5.0 \times 10^{-7}$  s, and one at half the baseline time step,  $1.25 \times 10^{-7}$  s. Each case was computed to a final computational time of 0.25 s. Table 2 shows the collision rates for the three cases. There is very little difference between all of the collision rates between the three cases with the differences between the cases most certainly associated with the statistical scatter associated with these types of schemes. Notice that halving or doubling the step size approximately doubled or halved the amount of time required to calculate the solution.

Table 2. Collision Rates for Solution Convergence Cases

Scheme	Compute Time [hr]	Time Step [s]	Total Collisions [# /s]	Xe-Xe <sup>+</sup> Charge Exchange [# /s]	Xe-Xe Elastic [# /s]	Xe-Xe <sup>+</sup> Elastic [# /s]
SCN	107.2	$1.25 \times 10^{-7}$	$5.301 \times 10^7$	$5.046 \times 10^7$	$2.519 \times 10^5$	$2.293 \times 10^6$
SCN	58.9	$2.5 \times 10^{-7}$	$5.325 \times 10^7$	$5.069 \times 10^7$	$2.560 \times 10^5$	$2.303 \times 10^6$
SCN	30.9	$5.0 \times 10^{-7}$	$5.310 \times 10^7$	$5.056 \times 10^7$	$2.541 \times 10^5$	$2.287 \times 10^6$

Figure 2 shows the evolution of the total number of neutrals and ions as well as the total number of particles. These counts are nearly identical with any differences with the statistical scatter.

Figure 3 shows the final number density for the neutrals for the three cases. Figure 4 shows the final number density for the ions for the three cases, and Figure 5 shows the final electrostatic potential for the three cases. All of these again show on very minor differences between the three cases, and these are when the number densities are low and are associated with the statistical scatter. The outer wings of the plume are captured in all three cases as can be seen in the ion number density and the electrostatic potential. The time step is sufficient to capture the ion curved trajectories as is shown behind the plasma source with ions occupying some of the region behind the plasma source. The very low ion density just behind the ion source is due to the ions colliding with that surface and reflecting back as accommodated neutrals.

Next, the local properties of the plasma will be compared between the three cases. The neutral sampling within in the plume is shown in Figure 6 for both the velocity distribution as well as the speed distribution,

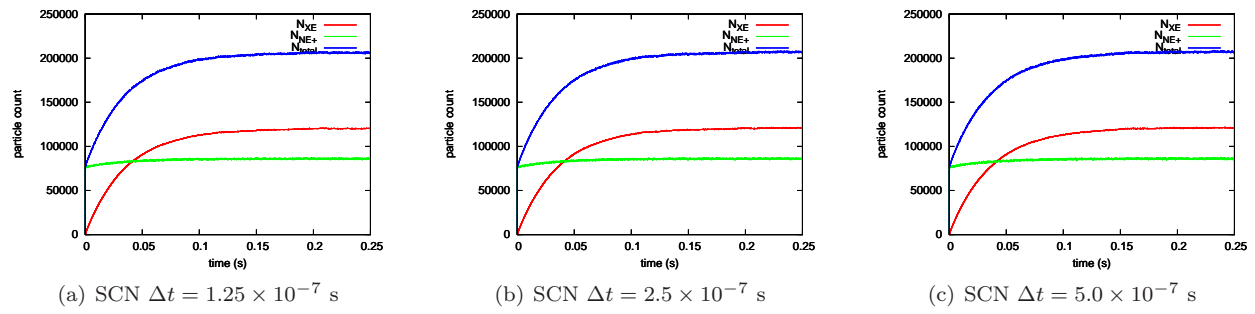


Figure 2. Global Particle Counts for Solution Convergence Cases

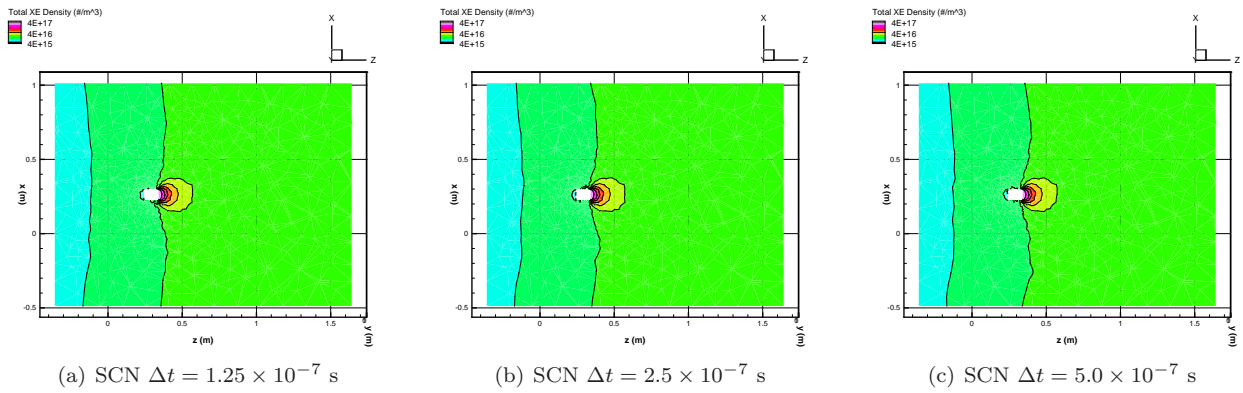


Figure 3. Final Neutral Number Density for Solution Convergence Cases

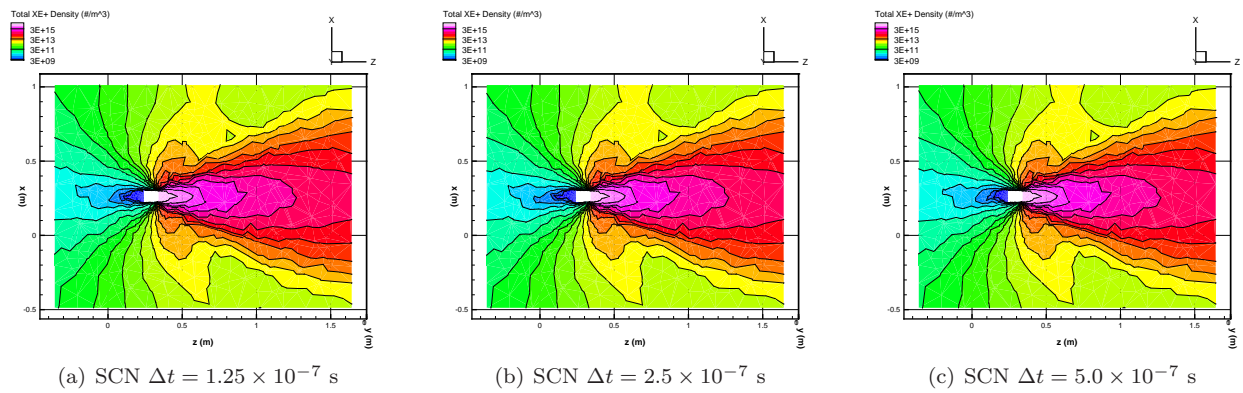
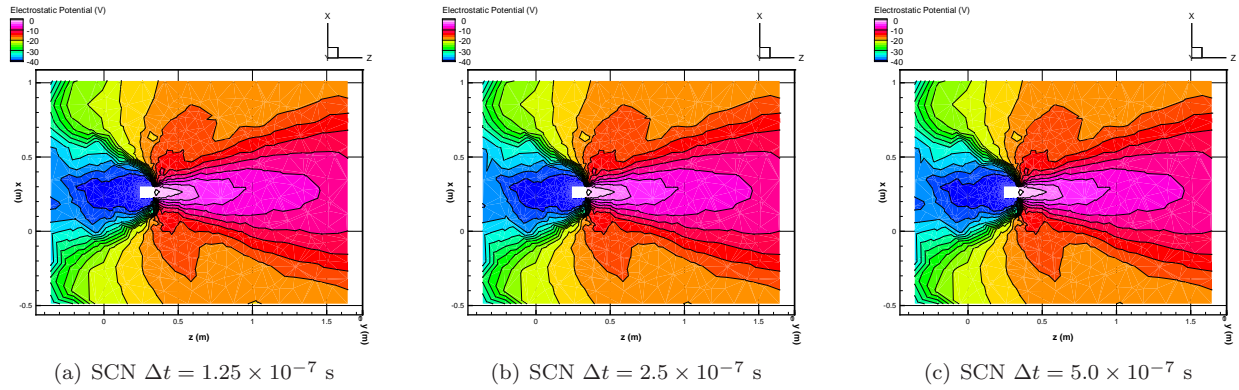
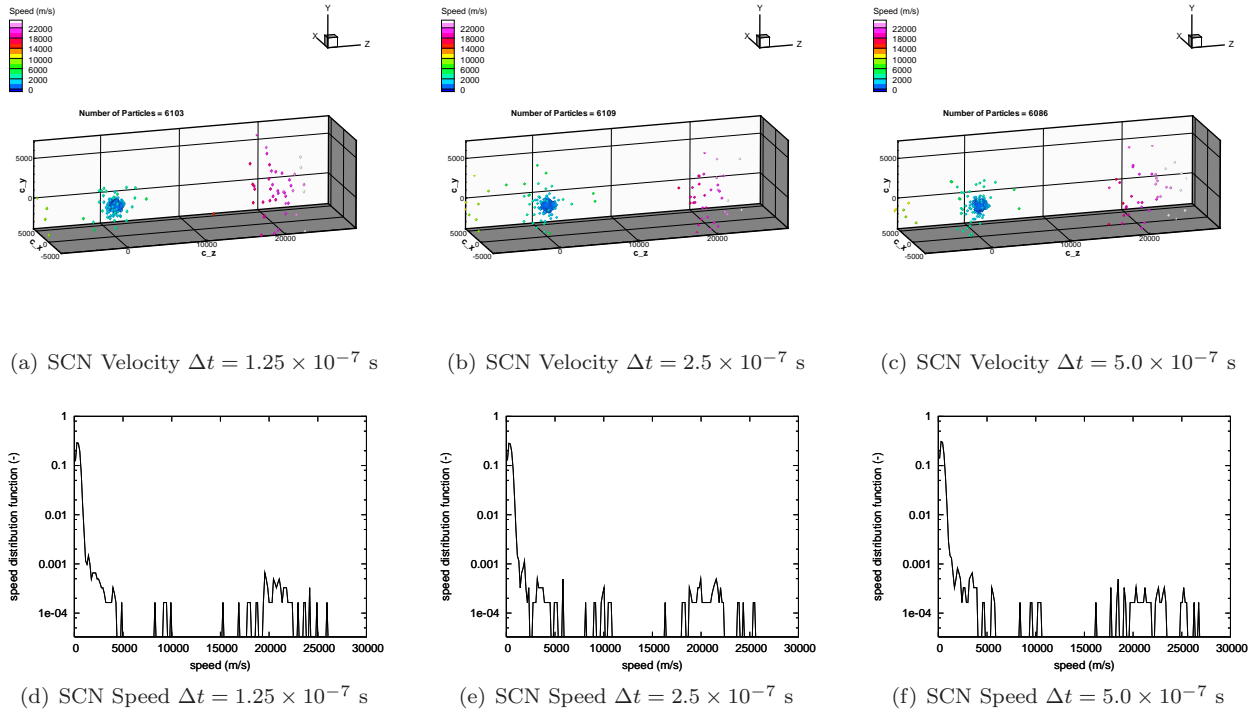


Figure 4. Final Ion Number Density for Solution Convergence Cases



**Figure 5. Final Electrostatic Potential for Solution Convergence Cases**

where the velocity distribution is showing the outer edge of the velocity space domain that is populated with particles and the surfaces are colored by z-velocity since that is the primary velocity direction. Figure 7 shows the ion sampling within the plume. Once again, there is very little differences between the three cases. A bimodal distribution is seen in the ion distribution with the lower speed ions being the result of the charge-exchange collisions between the neutrals and the ions. The corresponding high speed neutrals can be seen in the neutral distributions, but the clarity is obscured because of the relative low occurrence of the particles compared to the computational particle weighting used for the neutrals.



**Figure 6. Neutral Velocity and Speed Distributions 0.1 m in Front of Thruster for Solution Convergence Cases**

The neutral sampling outside the plume is shown in Figure 8 for both the velocity distribution as well as the speed distribution. Figure 9 shows the ion sampling outside the plume. In this case there is very little difference between the three cases, but some minor differences do occur. The majority of the neutrals that are being sampled in this region are most likely from the reflected from the walls. That is why the most probable velocity is so low. However, the  $5.0 \times 10^{-7}$  s case does show some added noise in the higher velocities. Notice that at this time step, we are very close to the ion characteristic time step, so the increase in the time step size might have altered the ion trajectories enough to alter the neutral distribution in the

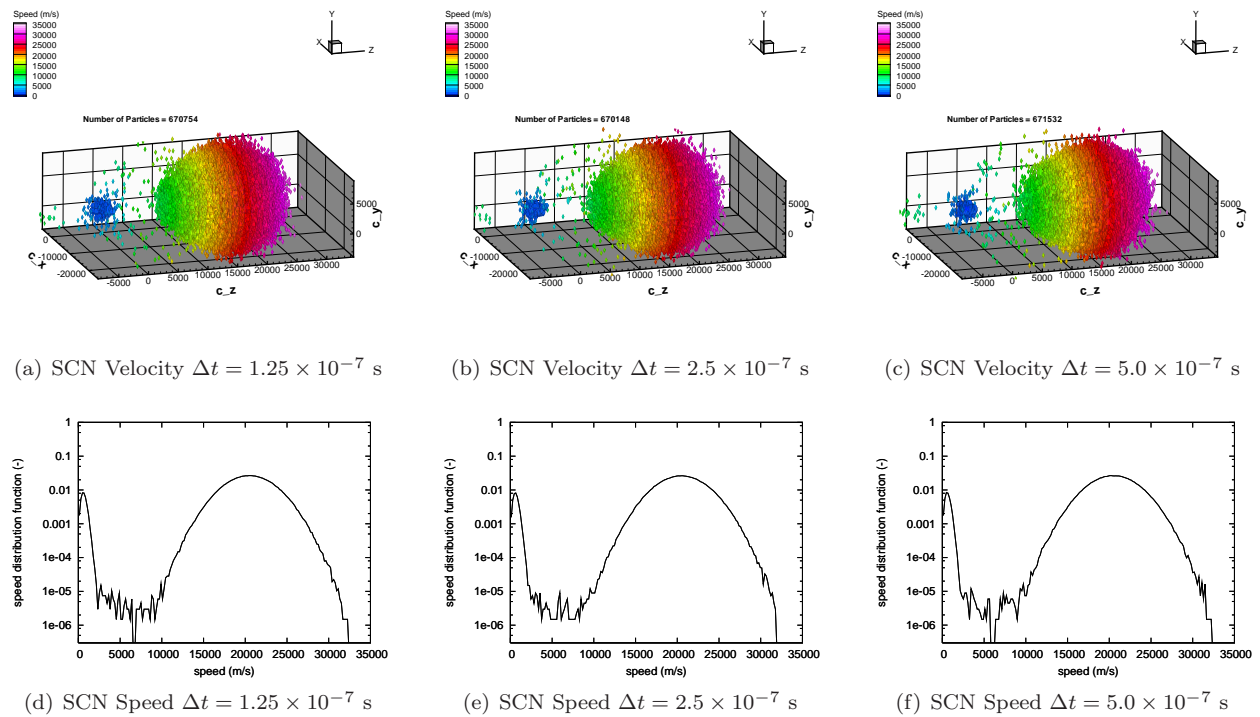


Figure 7. Ion Velocity and Speed Distributions 0.1 m in Front of Thruster for Solution Convergence Cases

higher speeds. There still exists a bimodal distribution in the ion velocity, but the number of low speed ions is significantly less than what were in front of the thruster. Also, the most probable speed of the ions has dropped from the 20 km/s that it was in front of the thruster to around 4 km/s. This is because the ions that make it to this region of the flow are the low speed charge exchange ions that have been accelerated through the electrostatic potential field into this region.

### C. Coarse Time Step Solution

Now the coarse time step case can be compared to the fine time step. For this case all particles and physical processes are propagated at a time step of  $2.5 \times 10^{-5}$  s. From the previous discussions, it is known that this time step is larger than the characteristic time associated with the electrostatic forces,  $5.0 \times 10^{-5}$  s, and is very close to the smallest characteristic time associated with the collision modeling,  $4.7 \times 10^{-5}$  for the high speed neutrals and ions charge exchange collisions. Table 3 shows the resulting collision rates along with the fine time step collision rates.

Table 3. Collision Rates for Coarse Time Step

	Compute	Time	Total	Xe-Xe <sup>+</sup> Charge	Xe-Xe	Xe-Xe <sup>+</sup>
Scheme	Time [hr]	Step [s]	Collisions [# /s]	Exchange [# /s]	Elastic [# /s]	Elastic [# /s]
SCN	58.9	$2.5 \times 10^{-7}$	$5.325 \times 10^7$	$5.069 \times 10^7$	$2.560 \times 10^5$	$2.303 \times 10^6$
SCN	1.73	$2.5 \times 10^{-5}$	$4.945 \times 10^7$	$4.726 \times 10^7$	$2.572 \times 10^5$	$1.936 \times 10^6$

The first thing to notice from this figure is that taking 100 times fewer time steps results in a significant decrease in compute time, by a factor of around 34. Unfortunately, only the Xe-Xe elastic collision rate is the same between the coarse and fine time steps. The elastic and charge exchange collisions associated with the Xe-Xe<sup>+</sup> pairs. Therefore by not adequately resolving the ion trajectory there has been a decrease in the collision rate associated with the ions. This could be caused by the ions traveling entirely through the high density region in front of the plasma source (where collisions are most likely) before the ions can participate in a significant number of collision events. Taking the nominal ion velocity of 20 km/s and the time step of



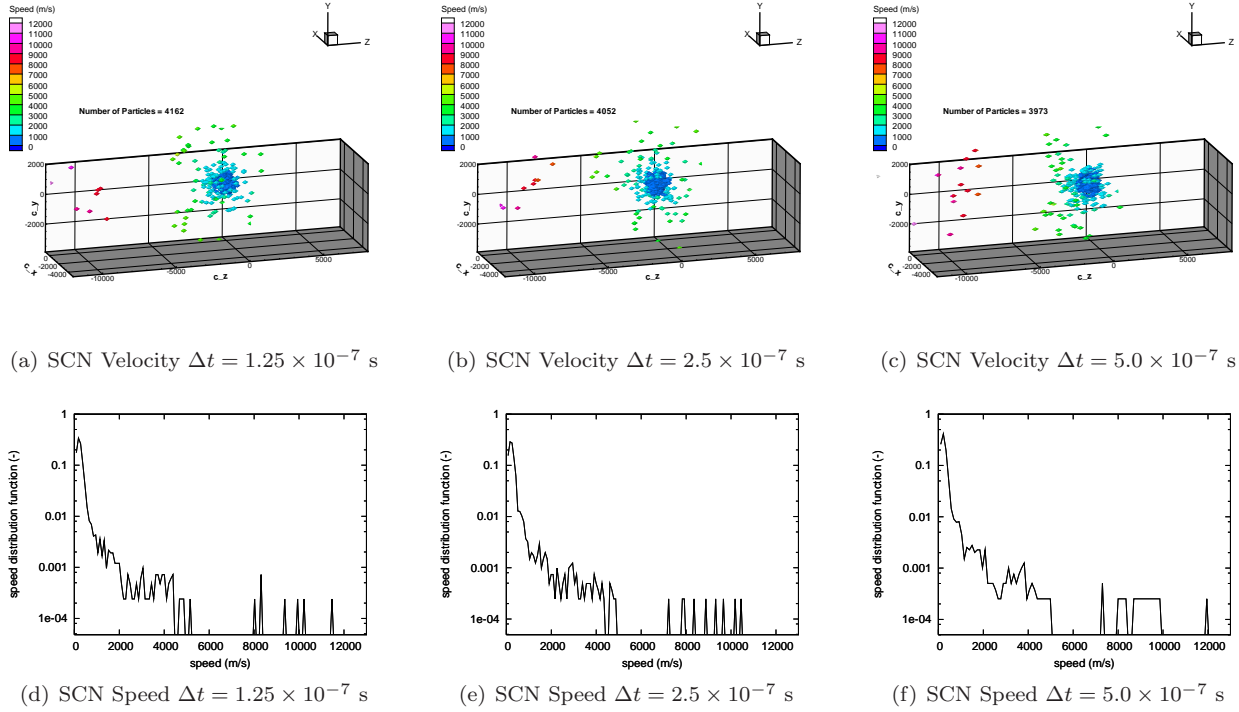


Figure 8. Neutral Velocity and Speed Distributions 0.28 m Above Thruster Face for Solution Convergence Cases

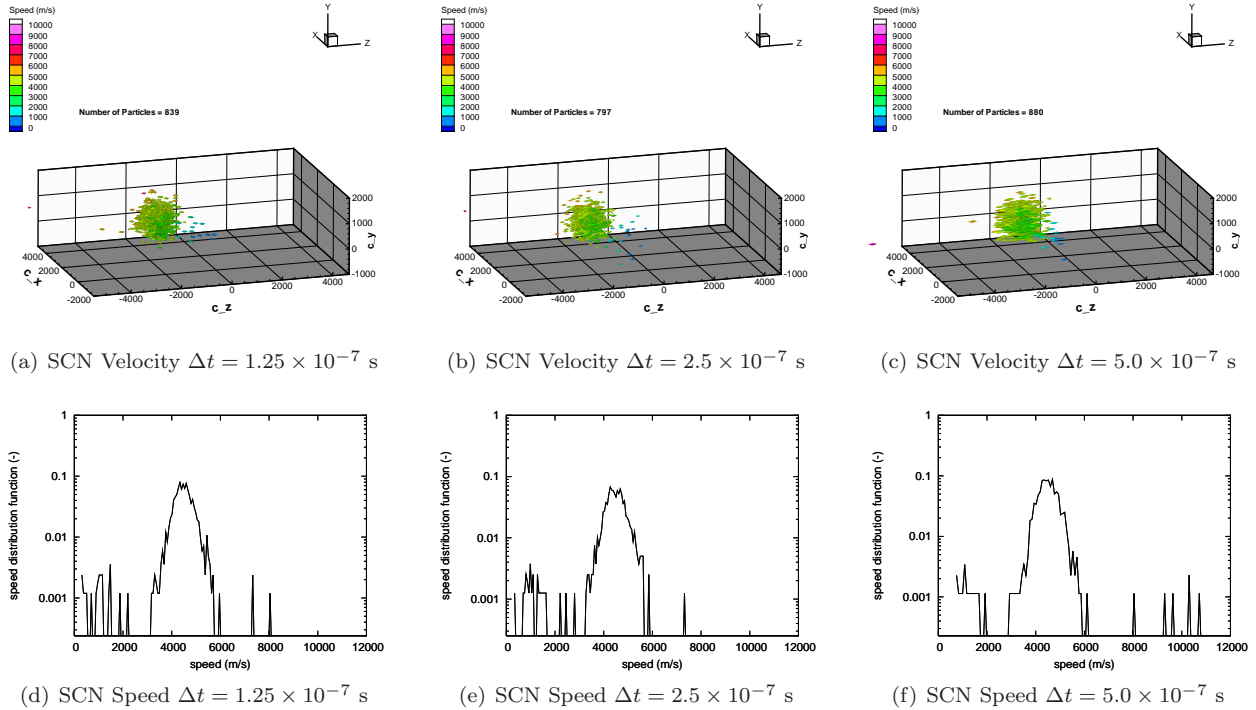


Figure 9. Ion Velocity and Speed Distributions 0.28 m Above Thruster Face for Solution Convergence Cases

$2.5 \times 10^{-5}$  s yields a distance traveled by an ion of 0.5 m. This is a significant distance from the plasma source and is certainly outside of the high density region, compare this with where the high density regions were in the fine time step cases from Figures 3 and 4.

While significant differences are seen in the collision rates, Figure 10 shows the evolution of the total number of neutrals and ions as well as the total number of particles is very similar. Thus, the differences between the two cases must be for only a small, but significant, fraction of the total particles.

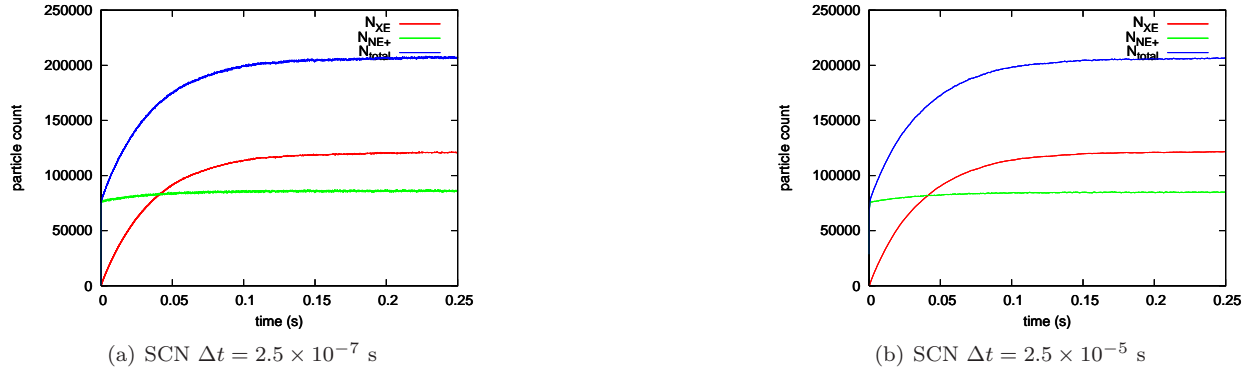


Figure 10. Global Particle Counts for Coarse Time Step

Figure 11 shows the final number density for the neutrals for the coarse and fine time step cases. Even for this case the neutral number density is fairly similar. It appears that the coarse time step does not have a significant effect on the overall neutral number density. This does not mean, however, that there is no effect. Since the collision rate is different, there might be some difference that might not be observable in this figure.

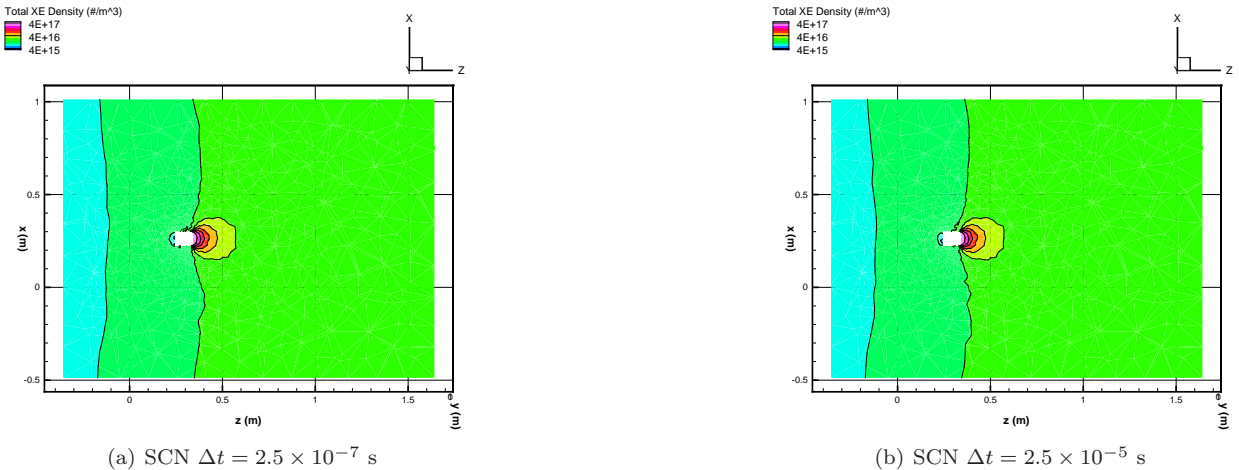


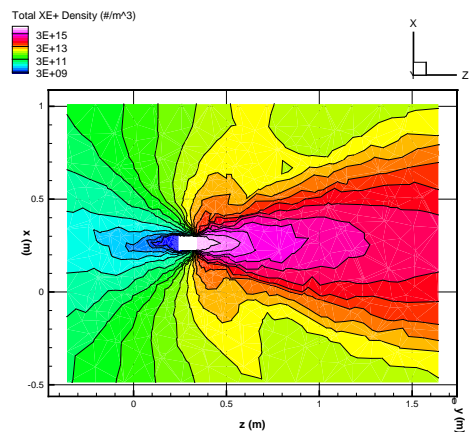
Figure 11. Final Neutral Number Density for Coarse Time Step

Figure 12 shows the final number density for the ions for the coarse and fine time step cases. This shows a significant difference between the two cases. While the main beam region seems similar, the outer wings of the plume are certainly not captured as well in the coarse time step case. Also, with the time step so large, the ions cannot make the curved trajectory to collide with the back of the ion source, which results in the difference between to two cases in that region.

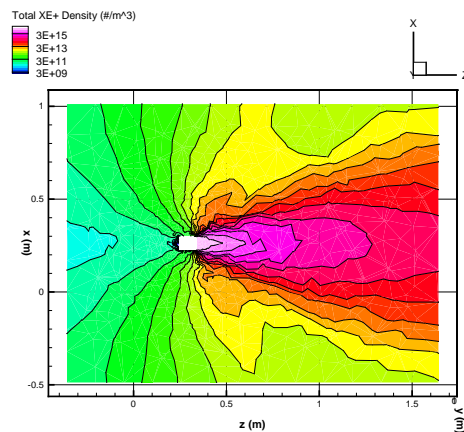
Figure 13 shows the final electrostatic potential for the coarse and fine time step cases. This again shows less accurate resolution of the outer wings of the plume region. Also an increased potential region behind the plasma source exists since the ions are not colliding with the back of the plasma source and becoming neutralized.

Next, the local properties of the plasma will be compared between the three cases. The neutral sampling within in the plume is shown in Figure 14 for both the velocity distribution as well as the speed distribution.



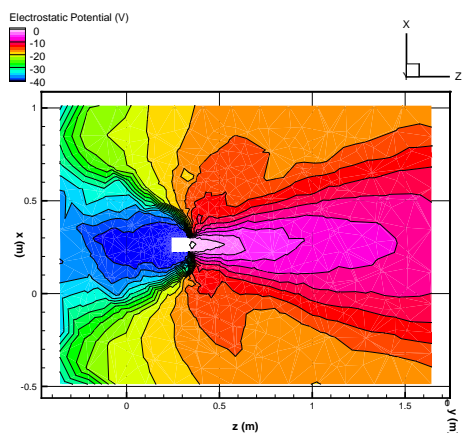


(a) SCN  $\Delta t = 2.5 \times 10^{-7}$  s

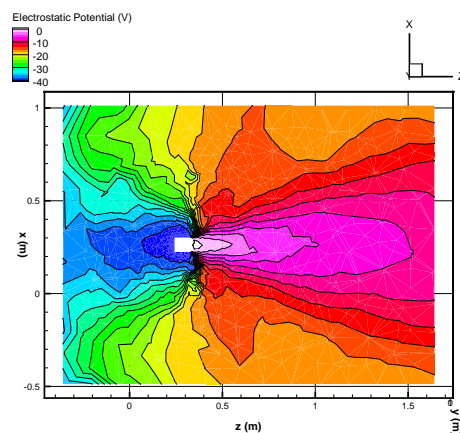


(b) SCN  $\Delta t = 2.5 \times 10^{-5}$  s

Figure 12. Final Ion Number Density for Coarse Time Step



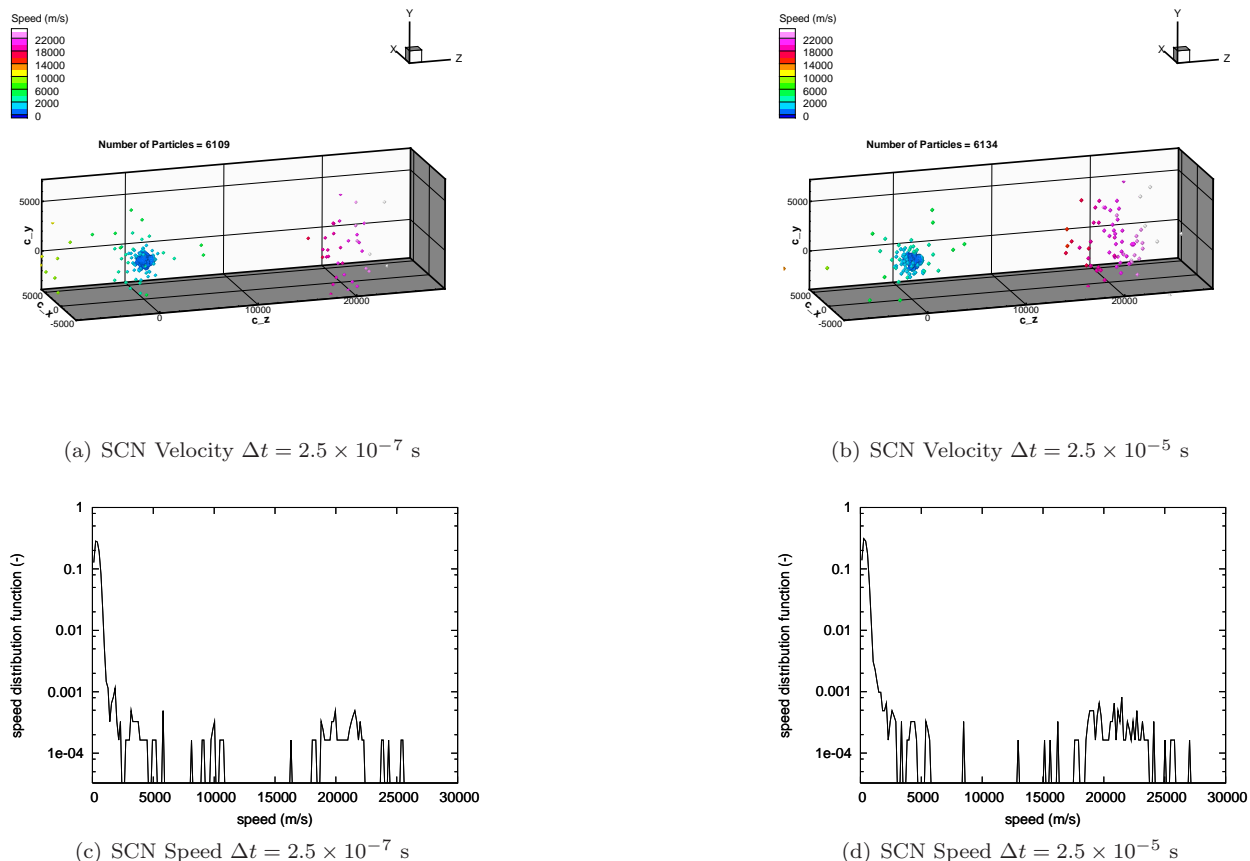
(a) SCN  $\Delta t = 2.5 \times 10^{-7}$  s



(b) SCN  $\Delta t = 2.5 \times 10^{-5}$  s

Figure 13. Final Electrostatic Potential for Coarse Time Step

The most significant difference here is that there is a significantly larger band of high velocity neutrals, around the 20–25 km/s range, with a noticeable decrease in population in the 10 km/s region for the coarse time step. The 20 km/s neutrals are results of the charge exchange collisions with the high speed ions. The 10 km/s neutrals are most likely from secondary collisions between the high speed neutral and the other particles. Thus with the large time step, the high speed neutrals are able to travel entirely through the high density region before another collision event occurs.

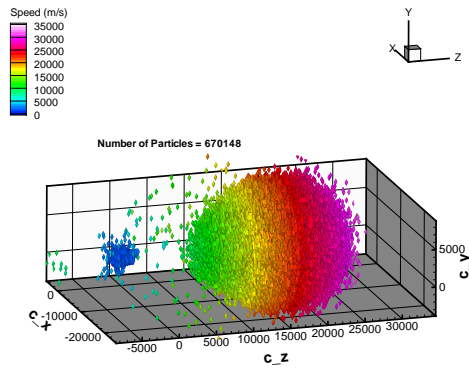


**Figure 14. Neutral Velocity and Speed Distributions 0.1 m in Front of Thruster for Coarse Time Step**

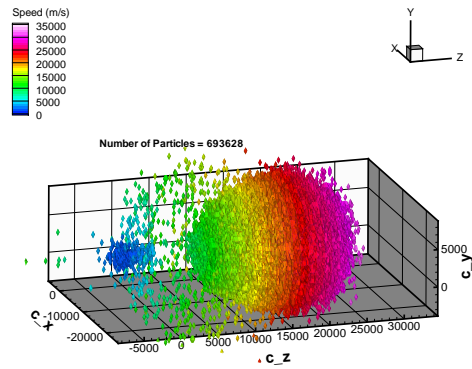
Figure 15 shows the ion sampling within the plume. Again a difference can be seen between the coarse and fine time step cases. First, there is a significant increase in the number of ions in between the two modes in the distribution. This velocity range, around 10 km/s, corresponds to the decrease in the distribution of neutrals mentioned above. It appears that with the coarse time step there is not enough charge exchange collisions occurring between the medium speed ions and neutrals. Notice that these ions are mainly produced by the charge exchange collisions from a previous time step since the plasma source is producing a Maxwellian distribution of ions with the peak of the distribution at 20 km/s. Thus it appears that the coarse time step is moving the particles out of the high density region too quickly.

The neutral sampling outside the plume is shown in Figure 16 for both the velocity distribution as well as the speed distribution. While the two distributions look similar, there is more concentrated collection of particles in the 8 km/s region for the coarse time step. This is hard to distinguish from the statistical scatter in the data, but this clustering does occur over 8 consecutive velocity bins, so this may be more than a statistical artifact.

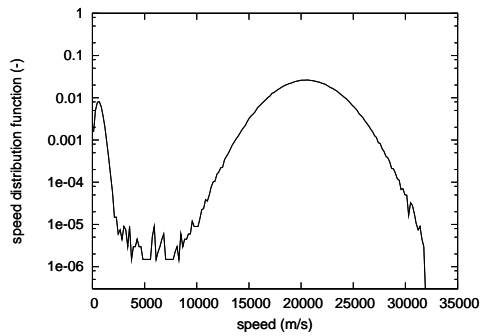
Figure 17 shows the ion sampling outside the plume. In this case there are significant differences between the coarse and fine time step cases. The most notable is that the coarse time step has a bimodal distribution with the second peak rather wide and centered around 10 km/s. This peak does not appear on the fine time step and must be a result of the coarse time step. Again, the speed is associated with secondary collisions, and if the fast moving particles, which are the only ones that create these particles, travel through the high density region before another collision event is performed, then there would be left over medium speed ions.



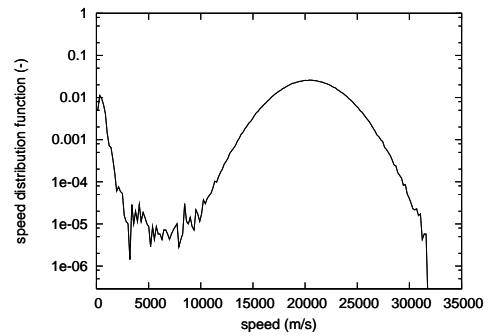
(a) SCN Velocity  $\Delta t = 2.5 \times 10^{-7}$  s



(b) SCN Velocity  $\Delta t = 2.5 \times 10^{-5}$  s

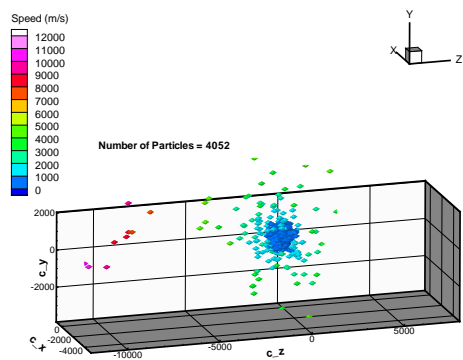


(c) SCN Speed  $\Delta t = 2.5 \times 10^{-7}$  s

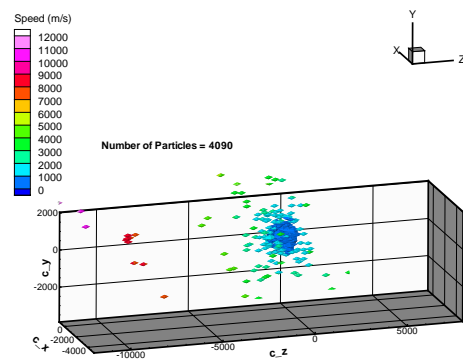


(d) SCN Speed  $\Delta t = 2.5 \times 10^{-5}$  s

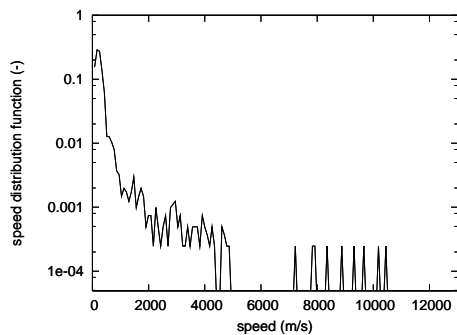
Figure 15. Ion Velocity and Speed Distributions 0.1 m in Front of Thruster for Coarse Time Step



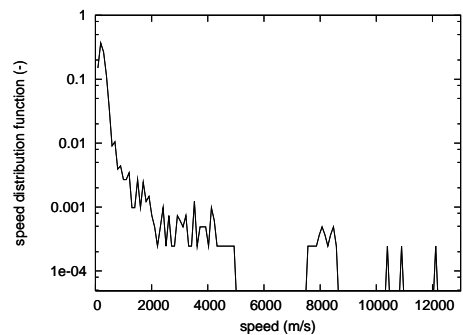
(a) SCN Velocity  $\Delta t = 2.5 \times 10^{-7}$  s



(b) SCN Velocity  $\Delta t = 2.5 \times 10^{-5}$  s



(c) SCN Speed  $\Delta t = 2.5 \times 10^{-7}$  s



(d) SCN Speed  $\Delta t = 2.5 \times 10^{-5}$  s

Figure 16. Neutral Velocity and Speed Distributions 0.28 m Above Thruster Face for Coarse Time Step

Also, the width of the main peak, that is center at 4 km/s is much larger for the coarse time step than for the fine time step. There is also a corresponding increase in the speed distribution function value at the peak. Again since this peak is a result of multiple collisions the coarser time step can again attribute this difference.

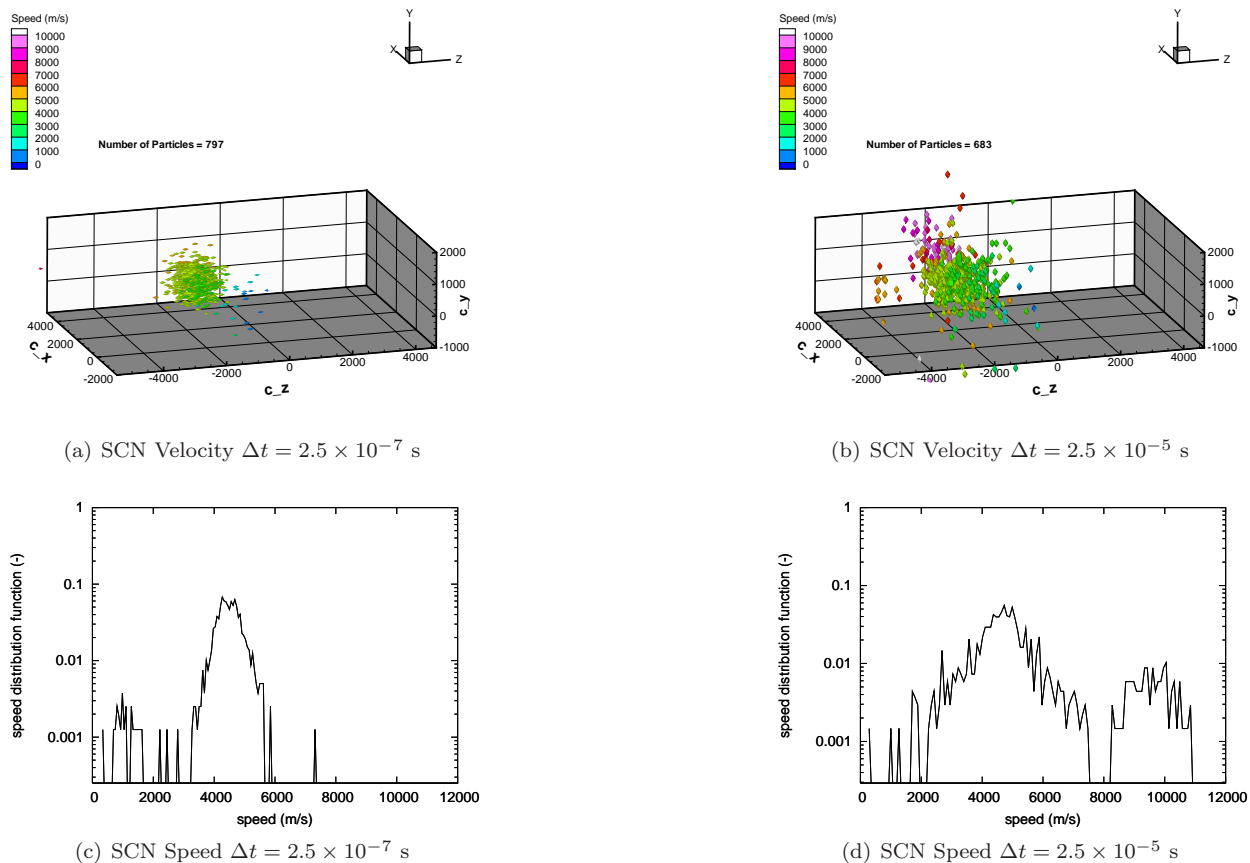


Figure 17. Ion Velocity and Speed Distributions 0.28 m Above Thruster Face for Coarse Time Step

It appears that there is a significant coupling between the particle time step and the ability to capture all of the secondary collisions that are occurring. Even though the time step was fine enough for the collision modeling characteristic time step, it appears that the rapid particle density variation in front of the plasma source is causing the collision characteristic time step calculation to be too large. Also, notice that while some of these effects are noticeable in the gross perspective of the flow field, the significant differences are only apparent with the observation of the velocity distribution functions.

#### D. Subcycling Solution

Now that is apparent the the coarse time step does not capture a number of significant flow features, an analysis of the improvements associated with the subcycling algorithm can be performed. The subcycling algorithm uses the coarse time step,  $2.5 \times 10^{-5}$  s, for the slow particle time step (i.e., slow neutrals) and the fine time step,  $2.5 \times 10^{-7}$  s, for the fast particle time step (i.e., for the fast ions and neutrals). Table 4 shows the resulting collision rates along with the fine and coarse time step collision rates for comparison.

The first thing to notice from this figure is that the subcycling scheme results in a decrease of computational time from 58.9 hr to 13.7 hr compared to the fine time step case. Unfortunately, the collision rates are nearly identical to the coarse time step rates and are significantly lower than the fine time step results (with the same exception of the Xe-Xe elastic collision rate).

While significant differences are seen in the collision rates, Figure 18 shows the evolution of the total number of neutrals and ions as well as the total number of particles is very similar. Thus, the differences

Table 4. Collision Rates for Subcycling Case

Scheme	Compute Time [hr]	Time Step [s]	Total Collisions [# /s]	Xe-Xe <sup>+</sup> Charge Exchange [# /s]	Xe-Xe Elastic [# /s]	Xe-Xe <sup>+</sup> Elastic [# /s]
SCN	58.9	$2.5 \times 10^{-7}$	$5.325 \times 10^7$	$5.069 \times 10^7$	$2.560 \times 10^5$	$2.303 \times 10^6$
SCN	1.73	$2.5 \times 10^{-5}$	$4.945 \times 10^7$	$4.726 \times 10^7$	$2.572 \times 10^5$	$1.936 \times 10^6$
SCY	17.3	$2.5 \times 10^{-5}$	$4.966 \times 10^7$	$4.745 \times 10^7$	$2.535 \times 10^5$	$1.963 \times 10^6$

between the subcycling case and the fine time step case again must be for only a small, but significant, fraction of the total particles.

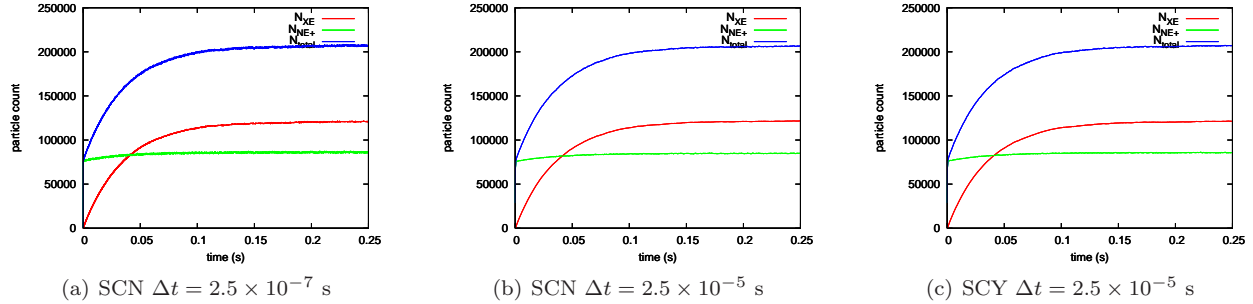


Figure 18. Global Particle Counts for Subcycling Case

Figure 19 shows the final number density for the neutrals for the subcycling case as well as the fine and coarse time step cases. This case again shows that there is little difference between the neutral number densities for the subcycling case. Thus, the overall neutral distribution is fairly insensitive to the computational time step. However, as was the case for the coarse time step, it is expected that there will be differences that are not observable in this perspective.

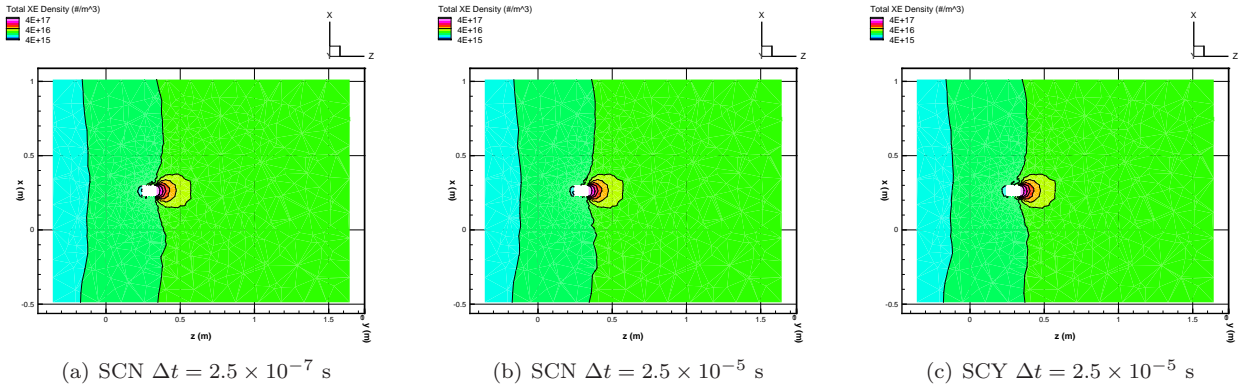


Figure 19. Final Neutral Number Density for Subcycling Case

Figure 20 shows the final number density for the ions for the subcycling case as well as the fine and coarse time step cases. Unlike the coarse time step case, the ion number density is very close to the fine time step case. The outer wings of the plume are captured, and the ion neutralization at the back of the plasma source is also captured. Therefore, the subcycling is drastically improving the capabilities of capturing the ion distribution.

Figure 21 shows the final electrostatic potential for the subcycling case as well as the fine and coarse time step cases. This again shows that the subcycling case and the fine time step cases are quite similar. This is to be expected since the electrostatic potential is directly related to the ion distribution. Even the potential drop behind the thruster seen in the fine time step case is captured in the subcycling case.

While the collision rates are different, the subcycling case has so far improved the ion number density

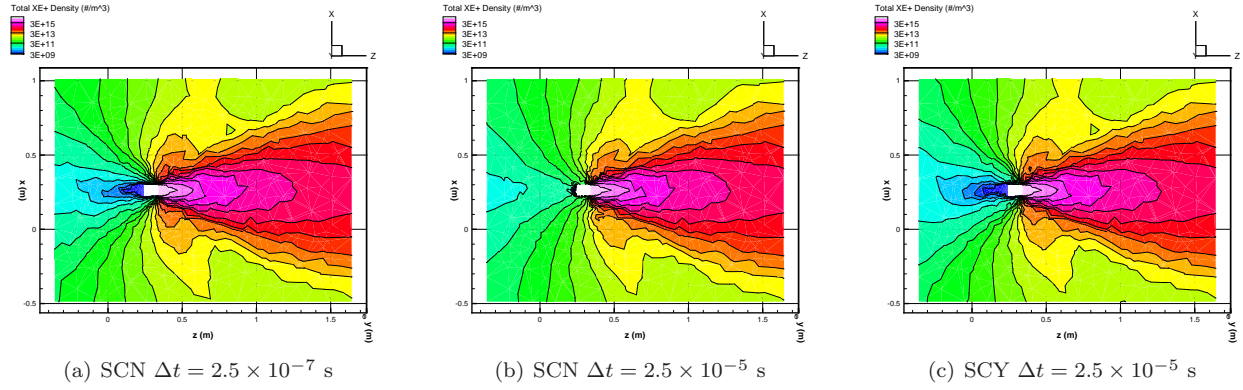


Figure 20. Final Ion Number Density for Subcycling Case

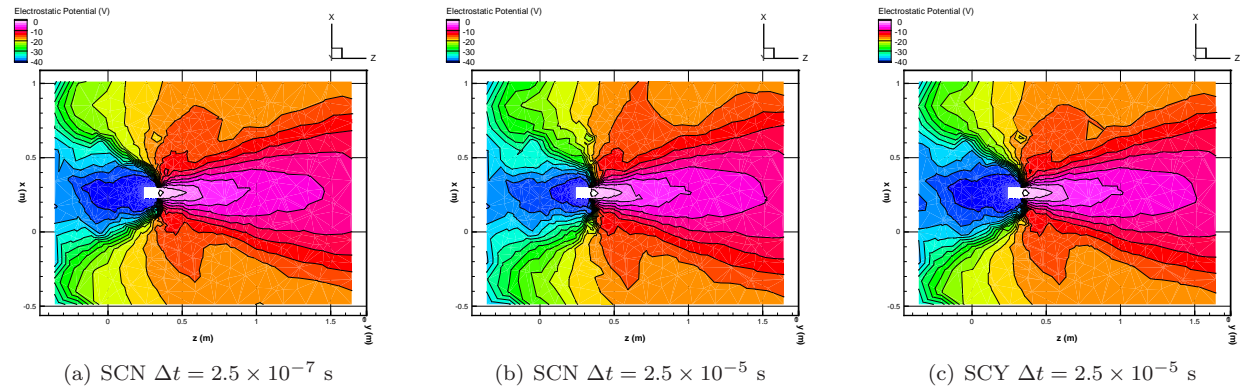
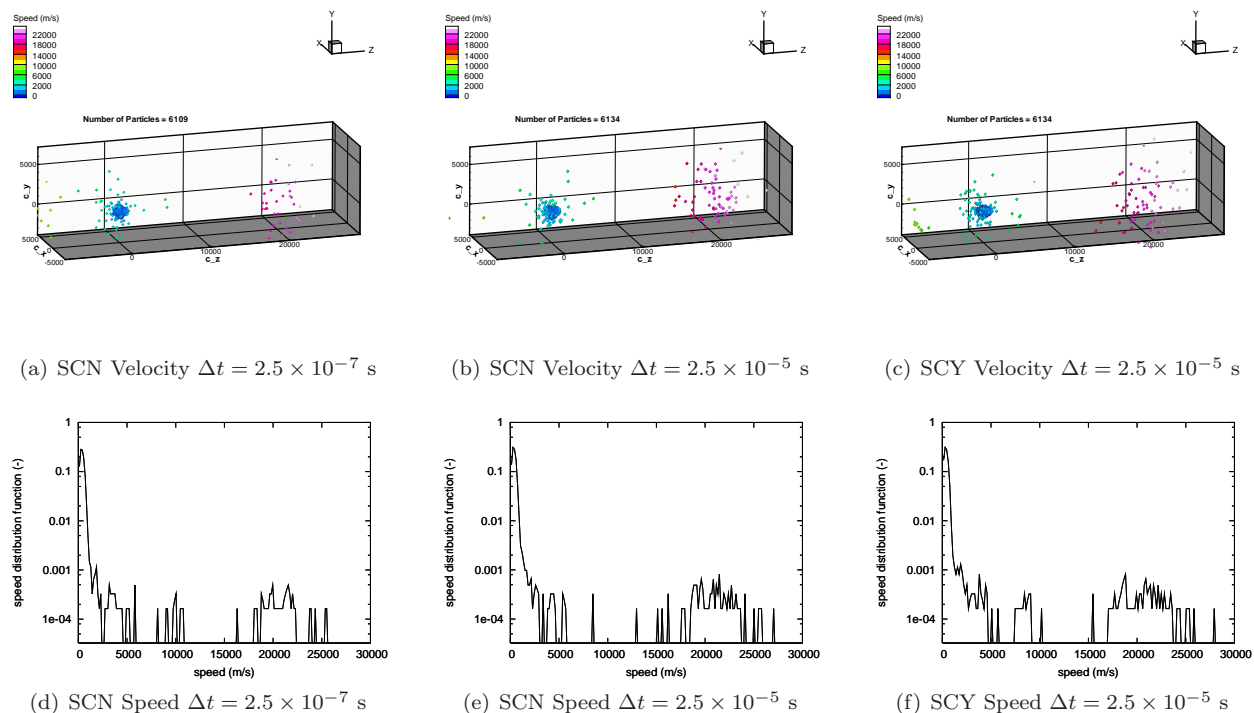


Figure 21. Final Electrostatic Potential for Subcycling Case

distribution compared to the coarse time step case and has shown no difference in the neutral number density distribution.

Next, the local properties of the plasma will be compared between the subcycling case and the fine and coarse. The neutral sampling within in the plume is shown in Figure 14 for both the velocity distribution as well as the speed distribution. Unfortunately, the subcycling cases looks much more similar to the coarse time step case and has significant differences with the fine time step case. The same arguments about the coarse time step differences also seem to apply here. While the neutrals are propagating at the fine time step, there is still no mechanism to get these neutrals to participate in collision events while they reside in the high density regions.



**Figure 22. Neutral Velocity and Speed Distributions 0.1 m in Front of Thruster for Subcycling Case**

Figure 23 shows the ion sampling within the plume. This case also shows significant differences between the subcycling and fine time steps and is very similar to the coarse time step. It appears that the secondary collision discussion from above explains these differences.

The neutral sampling outside the plume is shown in Figure 24 for both the velocity distribution as well as the speed distribution. While it is not certain that the 8 km/s region in the coarse time step is caused by statistical scatter, it is worth noting that the subcycling case does not demonstrate this feature. Otherwise, the subcycling case looks very similar to the fine time step case.

Figure 25 shows the ion sampling outside the plume. This case shows drastic improvements from the coarse time step. The subcycling case does not have the secondary peak in the 10 km/s range and has a similarly narrow speed range around the most probable speed. It is apparent that the subcycling does significantly improve the particle modeling outside the high density plume region. This is most likely due to the fact that the trajectory of the high speed ions is significantly improved with the fine time step, and thus these high speed ions are more effected by the electrostatic potential field.

## IV. Conclusions

The acceleration subcycling acceleration scheme within the AQUILA plasma modeling module of COLISEUM was investigated to determine how effective it is in capturing the local plasma properties. First, the simulation was demonstrated to be capable of converging to a solution for a sufficiently fine time step. This solution was the used to compare the performance of the simulation at a much coarser time step. This



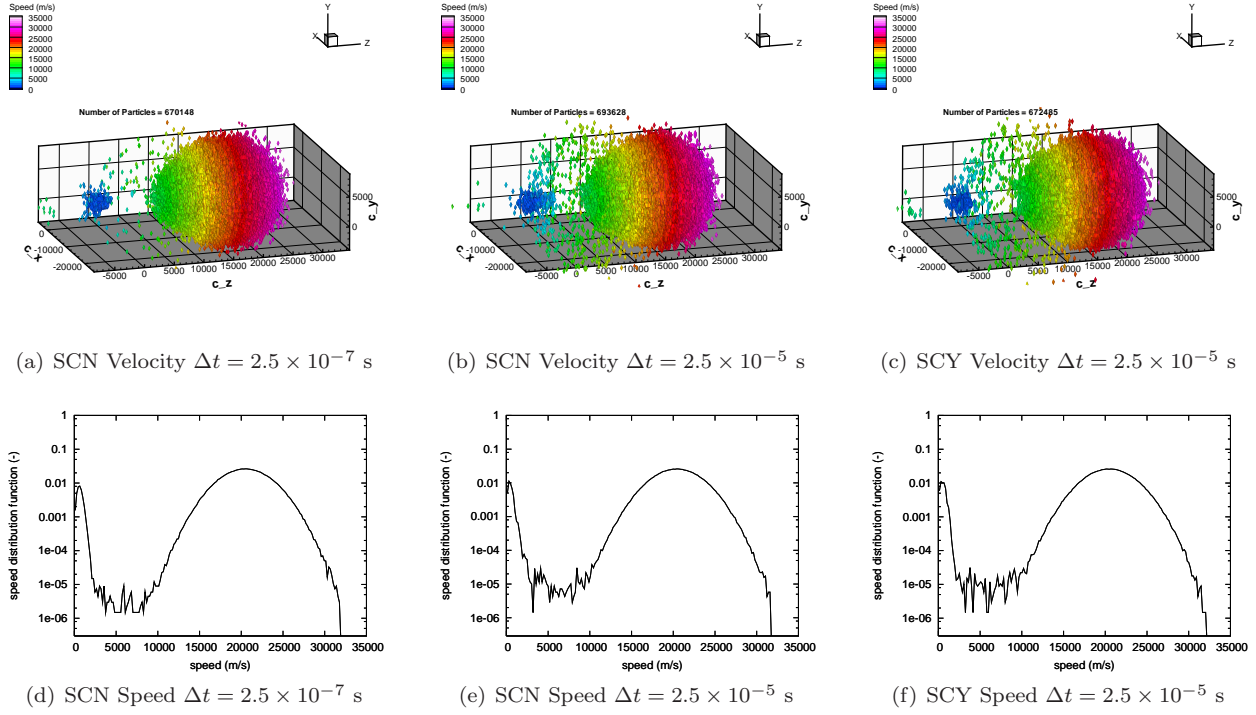


Figure 23. Ion Velocity and Speed Distributions 0.1 m in Front of Thruster for Subcycling Case

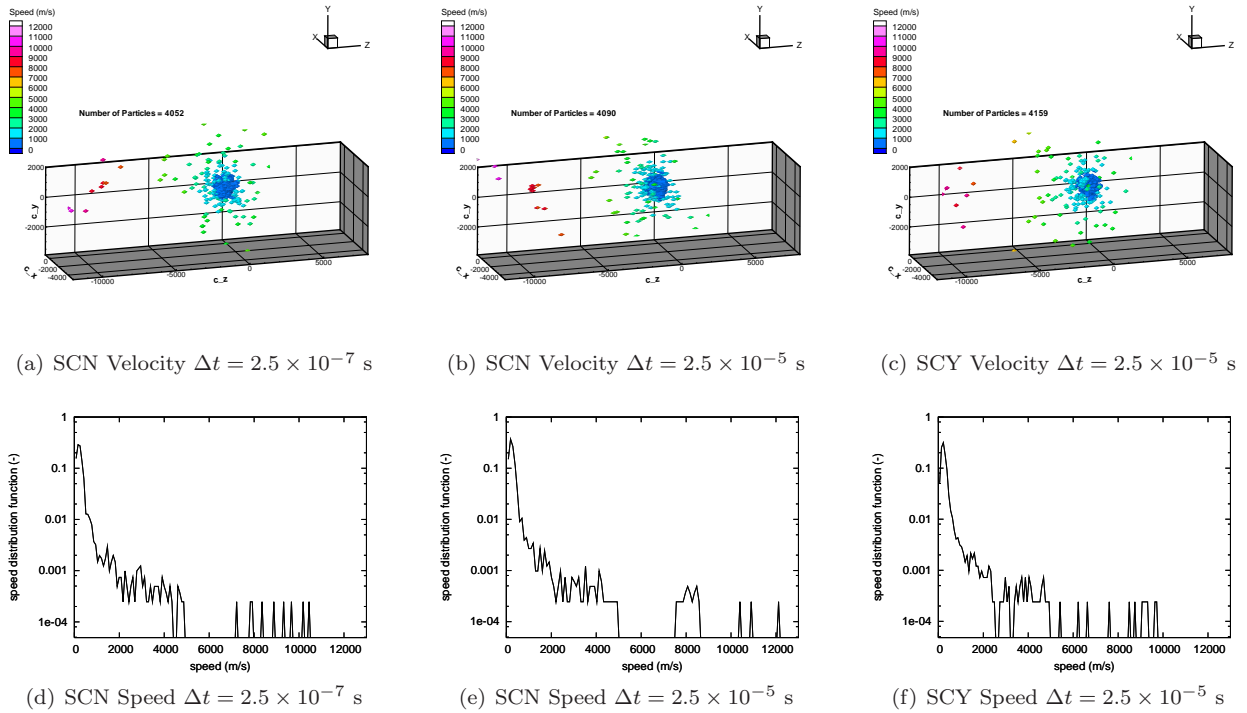
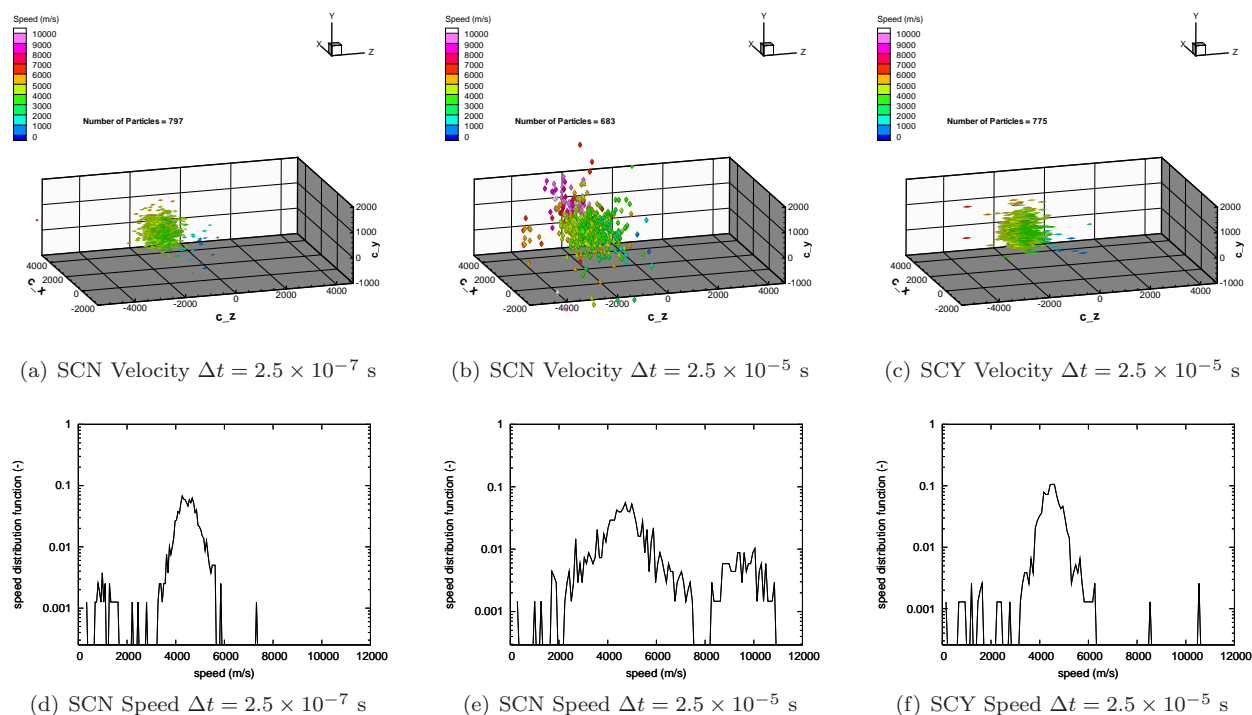


Figure 24. Neutral Velocity and Speed Distributions 0.28 m Above Thruster Face for Subcycling Case



**Figure 25. Ion Velocity and Speed Distributions 0.28 m Above Thruster Face for Subcycling Case**

showed several deficiencies in the coarse time step solution. These were mainly focused on the fact that the high speed particles are leaving the high density region where multiple collisions are expected to occur after one or two time steps. In addition the coarse time step resulted in the ion trajectories being significantly off which resulted in large differences in the ion density distribution compared to the fine time step case.

The subcycling case improved the modeling of the number densities of the ions and neutrals compared to the coarse time step simulation with a compute time speedup of a factor of 3.4. It also significantly improved the modeling of the lower density region outside the main plume. In this region the velocity distribution functions for the neutrals and ions were both very similar to the fine time step case. This shows that by improving the modeling of the electrostatic forces, via finer time steps to propagate the ions and the force calculations, does improve the modeling of the plasma. For the higher density region of the main beam of the plasma, the subcycling showed no improvement compared to the coarse time step solution. While this appears to be rooted in the fact that a high speed particle can travel through the entire high density plume region in one time step and thus not participate in the additional collisions that appear to produce the different features of the fine time step solution. An alternative explanation to this behavior could be that the collision model is not providing consistent results at the different time scales. Suppose the collision model was selecting too many collisions to occur at the finer time step because the selection criteria was slightly off. This would result in a non-physical increase in additional collisions that the high speed particles would be participating in. This would mean that the fine time step solution was not correct.

To further identify the root cause of this problem, it is apparent that the collision model with AQUILA needs to be further validated in order to assure that it is not producing a surplus of collision events as the time step is decreased. While the collision model has been reported to have been successful in previous studies,<sup>2,3,8,14</sup> a systematic validation of the collision model source code has not been found by the authors.

Another suggested improvement to address the remaining differences between the subcycling and the fine time step cases is to perform the collision modeling between the high speed particles and the rest of the particles within the subcycle loop. While this would significantly decrease the computational efficiency associated with this scheme, it should address the problems in the high density regions. Performing this modification would be a non-trivial task as the collision code would need to be modified to only perform certain collision pairing at certain times.

## References

- <sup>1</sup>Fife, J. M., Gibbons, M. R., Hargus, W. A., VanGilder, D. B., and Kirtley, D. E., “3-D Computation of Surface Sputtering and Redeposition Due to Hall Thruster Plumes,” *28<sup>th</sup> International Electric Propulsion Conference*, March 17–21 2003.
- <sup>2</sup>Santi, M., Cheng, S., Celik, M., Martinez-Sanchez, M., and Peraire, J., “Further Development and Preliminary Results of the Aquila Hall Thruster Plume Model,” *39<sup>th</sup> AIAA/ASEE/SAE/ASEE Joint Propulsion Conference*, No. AIAA-2003-4873, Huntsville, AL, July 20–23 2003.
- <sup>3</sup>Gibbons, M. R., Kirtley, D. E., VanGilder, D. B., and Fife, J. M., “Flexible Three-Dimensional Modeling of Electric Thrusters in Vacuum Chambers,” *39<sup>th</sup> AIAA/ASEE/SAE/ASEE Joint Propulsion Conference*, No. AIAA-2003-4872, Huntsville, AL, July 20–23 2003.
- <sup>4</sup>Gibbons, M. R., Santi, M., VanGilder, D. B., and Fife, J. M., “Simulation of Plasma Expansion Using a Two-Timescale Accelerated Particle-in-Cell Method,” *42<sup>nd</sup> AIAA Aerospace Sciences Meeting and Exhibit*, No. AIAA-2004-0154, Reno, NV, January 5–8 2004.
- <sup>5</sup>U.S. Air Force Research Laboratory, Rocket Propulsion Division, Spacecraft Branch, Edwards AFB, CA, *COLISEUM User’s Manual*, 2005.
- <sup>6</sup>Massachusetts Institute of Technology, Space Propulsion Laboratory, Cambridge, MA, *AQUILA User’s Manual*, 2004.
- <sup>7</sup>Brieda, L., *Development of the DRACO ES-PIC code and Fully-Kinetic Simulation of Ion Beam Neutralization*, Master’s thesis, Virginia Polytechnic Institute and State University, Blacksburg, VA, 2005.
- <sup>8</sup>Santi, M., *Hall Thruster Plume Simulation Using a hybrid-PIC Algorithm*, Master’s thesis, Massachusetts Institute of Technology, Cambridge, MA, 2003.
- <sup>9</sup>Roussel, J.-F., Bernard, J., and Garnier, Y., “Numerical Simulation of Induced Environment, Sputtering and Contamination of a Satellite Due to Electric Propulsion,” *2<sup>nd</sup> European Spacecraft Propulsion Conference*, Noordwijk, the Netherlands, May 27–29 1997.
- <sup>10</sup>Gardner, B., Davis, V. A., Katz, I., and J., M. M., “Hall Current Thruster Plume Modeling – A Diagnostic Tool for Spacecraft Subsystem Impact,” *39<sup>th</sup> Aerospace Sciences Meeting*, No. AIAA-2001-0964, Reno, NV, January 8–11 2001.
- <sup>11</sup>Nannenber, K., Khayms, V., Emgushov, B., and Werthman, L., “Validation of Hall Thruster Plume Sputter Model,” *37<sup>th</sup> AIAA/ASME/SAE/ASEE Joint Propulsion Conference*, No. AIAA-2001-3986, Salt Lake City, UT, July 8–11 2001.
- <sup>12</sup>Yamamura, Y., Itikawa, Y., and Itoh, N., “Angular Dependence of Sputtering Yields of Monoatomic Solids,” Tech. Rep. IPPJ-AM-26, Nagoya, Japan, 1983.
- <sup>13</sup>Birdsall, C. K. and Langdon, A. B., *Plasma Physics via Computer Simulation*, McGraw-Hill, New York, 1985.
- <sup>14</sup>Celik, M., Santi, M., Cheng, S., Martinez-Sanchez, M., and Peraire, J., “Hybrid-PIC Simulation of a Hall Thruster Plume on an Unstructured Grid with DSMC Collisions,” *28<sup>th</sup> International Electric Propulsion Conference*, March 17–21 2003.
- <sup>15</sup>Bird, G. A., *Molecular Gas Dynamics and the Direct Simulation of Gas Flows*, Oxford University Press, Oxford, 1994.
- <sup>16</sup>Oh, D. Y. and Hastings, D. E., “Experimental Verification of a PIC-DSMC Model for Hall Thruster Plumes,” *32<sup>nd</sup> AIAA/ASME/SAE/ASEE Joint Propulsion Conference*, No. AIAA-1996-3196, Lake Buena Vista, FL, July 1–3 1996.
- <sup>17</sup>Pullins, S., Chiu, Y.-H., Levandier, D. J., and Dressler, R. A., “Ion Dynamics in Hall Effect and Ion Thrusters – Xe<sup>+</sup> + Xe Symmetric Charge Transfer,” *38<sup>th</sup> Aerospace Sciences Meeting and Exhibit*, No. AIAA-2000-0603, Reno, NV, January 10–13 2000.